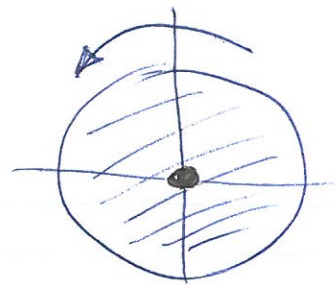


Plane problem - 2

# Rotating Disk (Axisymm. problem)



$\omega$  - ang. velocity

Material points have (normal) acceleration (non-rectilinear motion)

$$a_n = \frac{v^2}{r} = \omega^2 r$$

$\Rightarrow$  replace equilibrium in  $r$ -direction  $\Rightarrow$  eq. of motion:

force in  $r$ -direction per unit volume =  $-\rho a_n$

$\swarrow$  towards center

$$\frac{d\sigma_{rr}}{dr} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = -\rho\omega^2 r$$

Express  $\sigma$ 's in terms of  $\epsilon$ 's, and  $\epsilon$ 's in displacements.

$$\Rightarrow \boxed{\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{u}{r^2} = -(1-\nu^2) \frac{\rho\omega^2}{E} r}$$

$\swarrow$  non-homog. eq-n

General sol'n: (general, homog) + (particular, non-homog)

Homogeneous eq-n, general solution:  $u(r) = C_1 r + C_2 \frac{1}{r}$

Non-homog. (particular solution): try  $u \sim r^3 \Rightarrow$  works  
 $u = -(1-\nu^2) \frac{\rho\omega^2}{E} \frac{r^3}{8}$

∴ General sol'n:

$$U(r) = -\frac{\rho\omega^2(1-\nu^2)}{8E}r^3 + C_1r + C_2\frac{1}{r}$$

→ strains → Stresses:

$$\begin{cases} \sigma_{rr} = \frac{E}{1-\nu^2} \left[ -\frac{(3+\nu)(1-\nu^2)\rho\omega^2}{8E}r^2 + (1+\nu)C_1 - (1-\nu)\frac{C_2}{r^2} \right] \\ \sigma_{\theta\theta} = \frac{E}{1-\nu^2} \left[ -\frac{(1+3\nu)(1-\nu^2)\rho\omega^2}{8E}r^2 + (1+\nu)C_1 + (1-\nu)\frac{C_2}{r^2} \right] \end{cases}$$

Constants  $C_1, C_2$ : from b.c. - they depend on:  
solid disk or annular disk

Annular disk



$$\sigma_{rr} = 0 \quad \text{at } r = b \text{ (outer)}$$

$$\sigma_{rr} = 0 \quad \text{at } r = a \text{ (inner)}$$

They yield

$$C_1 = \rho\omega^2 \frac{a^2+b^2}{E} \frac{(1-\nu)(3+\nu)}{8}$$

$$C_2 = \rho\omega^2 \frac{a^2b^2}{E} \frac{(1+\nu)(3+\nu)}{8}$$

∴

$$\begin{cases} \sigma_{rr} = \frac{3+\nu}{8} \left( a^2+b^2 - r^2 - \frac{a^2b^2}{r^2} \right) \rho\omega^2 \\ \sigma_{\theta\theta} = \frac{3+\nu}{8} \left( a^2+b^2 - \frac{1+3\nu}{3+\nu}r^2 + \frac{a^2b^2}{r^2} \right) \rho\omega^2 \end{cases}$$

Max.  $\sigma_{rr}$ : from  $\frac{d\sigma_{rr}}{dr} = 0 \Rightarrow$  at  $r = \sqrt{ab}$

equals to  $\sigma_{rr}^{\max} = \frac{3+\nu}{8} (a-b)^2 \rho \omega^2$

$\rightarrow 0$  if  $b \rightarrow a$  is small

## Solid disk

$C_2 = 0$  (otherwise  $\sigma \rightarrow \infty$  at  $r=0$ )

$\sigma_{rr} = 0$  at  $r=b$

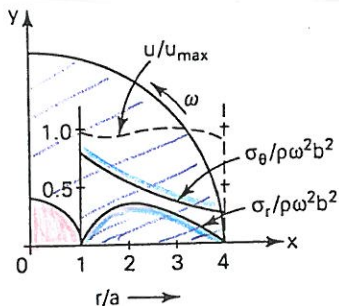
$\Rightarrow C_1 = \frac{(1-\nu)(3+\nu)}{8E} b^2 \rho \omega^2$

## Stresses :

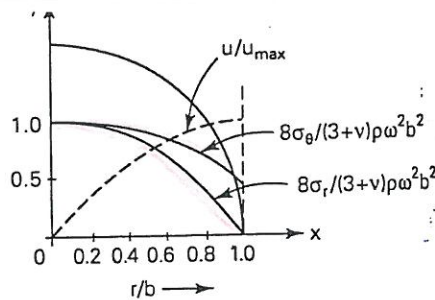
$\sigma_{rr} = \frac{3+\nu}{8} (b^2 - r^2) \rho \omega^2$  (max. at center)

$\sigma_{\theta\theta} = \frac{3+\nu}{8} \left( b^2 - \frac{1+3\nu}{3+\nu} r^2 \right) \rho \omega^2$

- hydrostat. at center  
 -  $\sigma_{\theta\theta} - \sigma_{rr} \nearrow$  with  $r$

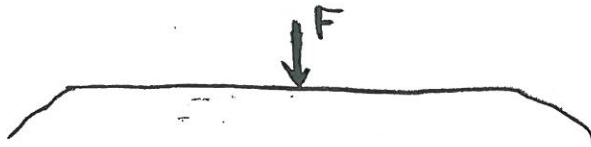


annular ( $\frac{a}{b} = 0.25$ )

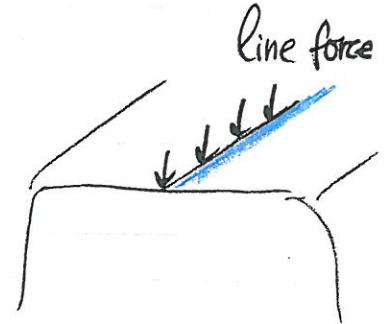


solid

# Normal force on boundary of half-plane



In the context of plane  $\epsilon$ :

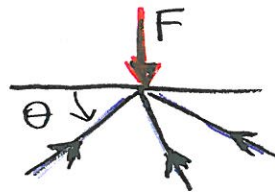


Importance:

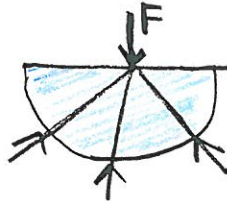


by integration of point force sol'n

Guess:  $\sigma_{rr}$  is the only stress:  $\sigma_{rr} = \sigma_{rr}(r, \theta)$



Eq-m of half-circle:



$$\int_0^{\pi} \overset{\text{compressive}}{-\sigma_{rr} \sin \theta} r d\theta = F$$

↑ const. when integrating

⇒ Seek  $\sigma_{rr}$  in the form

$$-\sigma_{rr} = \frac{F}{r} f(\theta)$$

↑ to be found

$$-\sigma_{rr} = \frac{F}{r} f(\theta)$$

Check eq-ns

• Equilibrium:  $\frac{\partial \sigma_{rr}}{\partial r} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = 0$  : satisfied for any  $f(\theta)$  no restrictions

• Compatibility: need to check since our guess is in stresses (not displacements)

Expressed in stresses,  
with account of  
eq-m  $\Rightarrow$

$$\nabla^2 (\sigma_{rr} + \sigma_{\theta\theta}) = 0$$

$$\frac{\partial^2 \sigma_{rr}}{\partial r^2} + \frac{1}{r} \frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \sigma_{rr}}{\partial \theta^2} = 0$$

Laplacian in  
cylindri coord

$$\Rightarrow f''(\theta) + f(\theta) = 0 \quad (1/r^3 \text{ factors out})$$

$\Downarrow$

$$f(\theta) = A \sin \theta + B \cos \theta$$

Symmetry:



$$\sigma_{rr}(\theta) = \sigma_{rr}(\pi - \theta) \Rightarrow B = 0$$

$$-\sigma_{rr} = A \frac{\sin \theta}{r} F$$

Equilibrates applied force:



$$\int_0^\pi -\sigma_{rr} \sin \theta \cdot r d\theta = F$$

$\Downarrow$

$$A = \frac{1}{\int_0^\pi \sin^2 \theta d\theta = \pi/2} \Rightarrow \left[ \sigma_{rr} = -\frac{2}{\pi} \frac{\sin \theta}{r} F \right]$$

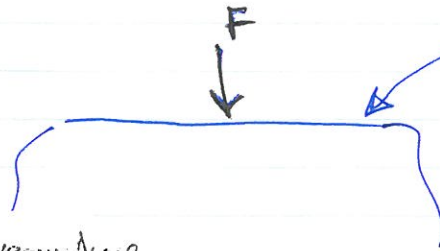
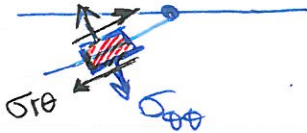
from eq. of half-circle

• Hooke's law : would give strains generated by  $\sigma_{rr}$  (as found)

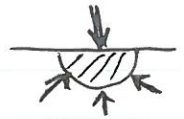
Boundary cond :

Satisfied

Since  $\sigma_{\theta\theta} = \sigma_{r\theta} = 0$  everywhere  
and, at boundary,



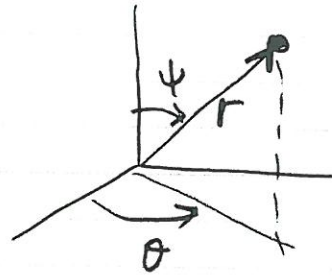
traction-free  
except one point  
where  $\sigma_{rr} \rightarrow \infty$



At point of  
infinite stress,  
the b. c.  
is satisfied in  
the integral sense  
for the domain



spherical coordinates:



$(r, \theta, \psi)$

Example of application: spherical shell under internal/external pressures

Radially-symmetric case:  $u_r \equiv u = u(r)$

is the only displac. component

$$\epsilon_{rr} = \frac{du}{dr}, \quad \epsilon_{\theta\theta} = \epsilon_{\psi\psi} = \frac{u}{r}$$

(similar to cylindrical)

Stresses: no shear stresses (symmetry)  $(\sigma_{r\theta} = \sigma_{r\psi} = \sigma_{\theta\psi} = 0)$

$\sigma_{rr}; \sigma_{\psi\psi} = \sigma_{\theta\theta}$  - normal stresses

Equilibrium:

$$\frac{d\sigma_{rr}}{dr} + 2 \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = 0$$

Expressing  $\sigma$ 's in terms of  $u$ ,

$$\frac{d}{dr} \left( \frac{du}{dr} + 2 \frac{u}{r} \right) = 0$$

unlike cylindrical

General sol'n:

$$u = Ar + B \frac{1}{r^2}$$

from b.c.

rather than  $\frac{1}{r}$  in cylindr.

